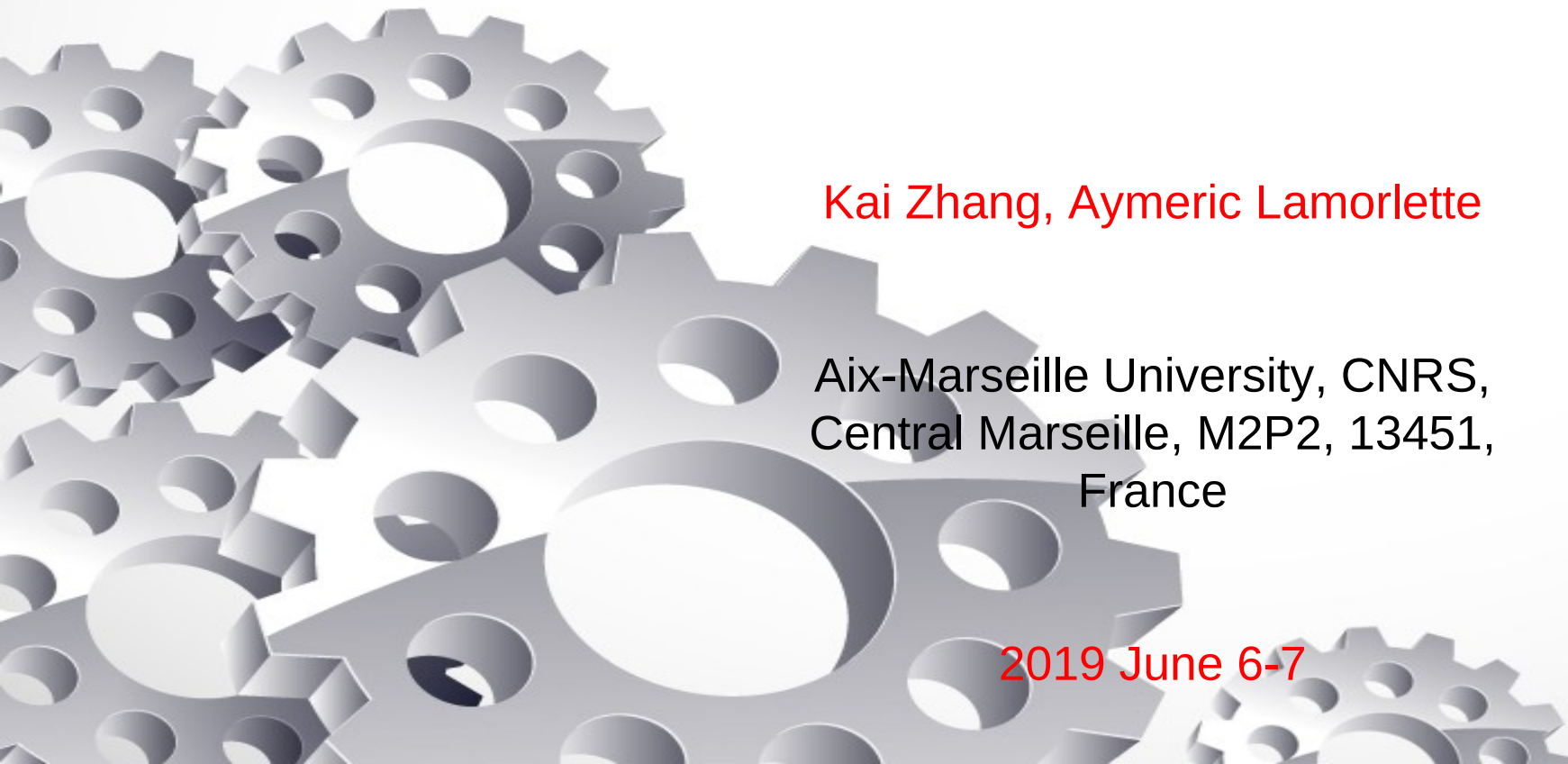


Role of vegetation density on wildland fire

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Motivation

Numerical configuration

Methodology

Results

Conclusions



- Is Froude number (Fr), Byram number (Nc) or other dimensionless number enough to describe fire behaviour?
- Lack of understanding of the effect of vegetation density ($CdLAI$) on
 - a. Fire regime transition from plume dominated to wind driven.
 - b. Heat transfer mechanism from radiative to convective heat transfer to ignite unburnt fuel.
- Lack of understanding of the configuration space $\{Nc, CdLAI\}$ effect on fire behaviour.

Sub-grid small-scale flame models is essential for large- or giga-scale fire modelling - *e.g.*, coupled fire-atmosphere modelling

Motivation

Numerical configuration

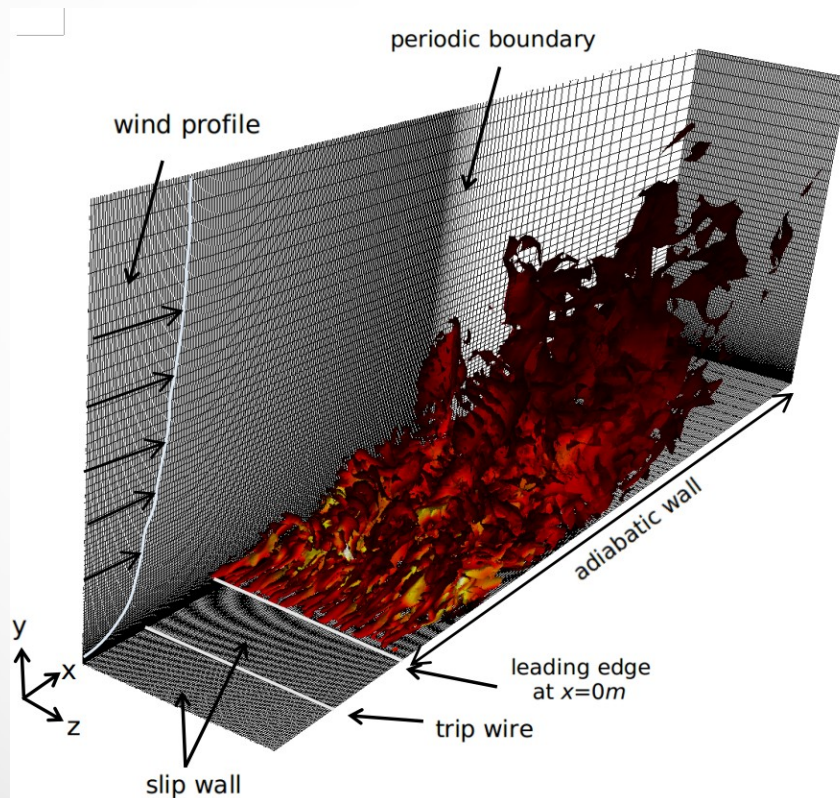
Methodology

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(Verma S. and Trouve A., 2018)



Solver: Simplified ForestFireFoam (FFF) developed from FireFoam at M2P2 Lab.

Features of FFF:

Multiphase turbulent combustion modelling with sub-models improvement for:

a. Pyrolysis; b. Evaporation; c. Char oxidation/Smoldering

d. Turbulent combustion:

- WALE;

- EDC;

e. Radiation: fvDOM

Utilities for pre- or post-processing:

- blockMesh; setFields; topoSet; funkySet, swak4Foam, paraview etc.

Visualization of the configuration using instantaneous iso-contour of Q -criterion at $2(s^{-2})$, clipped to $x_{max} = 2.5m$, $y_{max} = 1m$.



Question:

How does the configuration space $\{N_C, CdLAI\}$ determine flame regime (wind or plume dominated) and heat transfer to solid particle (radiation or convection governed)?

configuration space
 $\{N_C, CdLAI\}$

Byram convective number: $N_C = \frac{2gl}{\rho_\infty(U_\infty - ROS)^3 C_P T_\infty}$
 (Nelson, 2015)

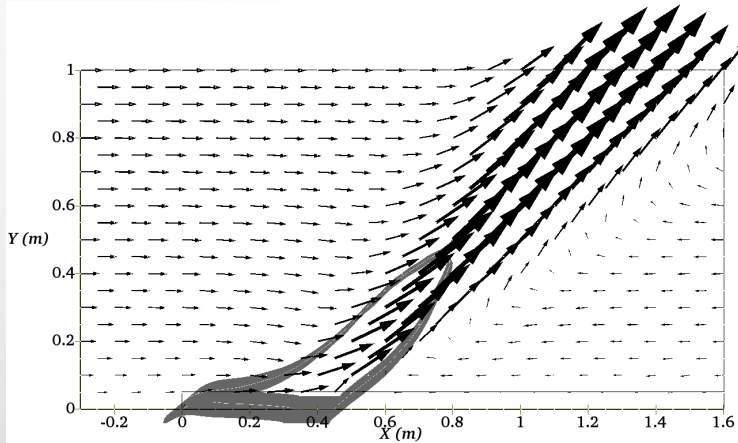
Drag Coefficient: C_d

(Lamorlette et al. 2015)

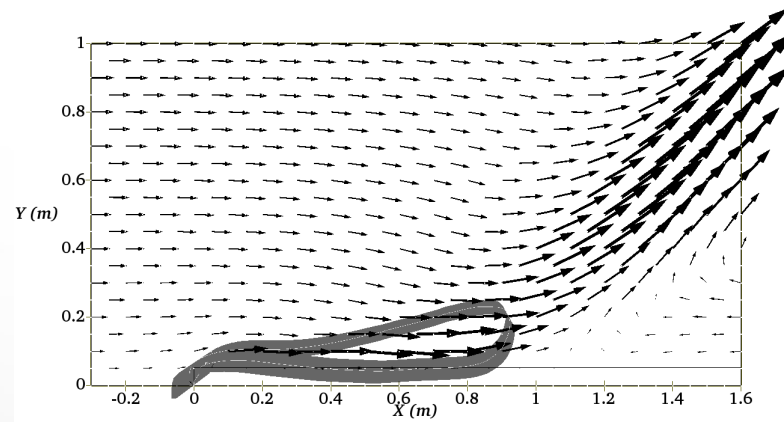
Leaf area index: $LAI \longleftrightarrow \alpha_s \sigma_s H_F / 2$

- $N_C < 2$ Wind, convection driven
- $2 < N_C < 10$ Mixed
- $N_C > 10$ Plume, radiation dominated
- Solid volume of fraction: α_s
- Surface to volume ratio: σ_s
- Vegetation height: H_F

500K 3D flame contour and velocity vectors:



$N_C=20, CdLAI=0.01$



$N_C=20, CdLAI=0.5$

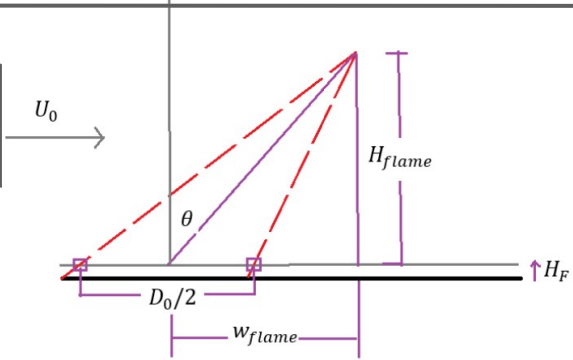
Nc alone is insufficient to describe fire behaviour!



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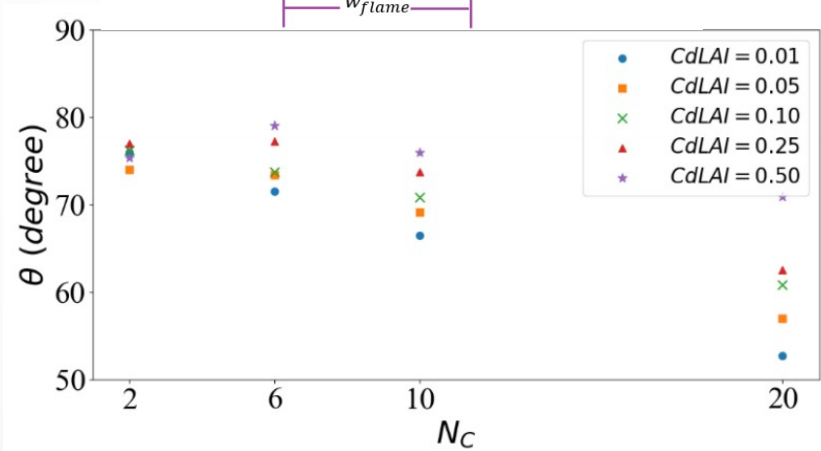
Flame tilt angle definition



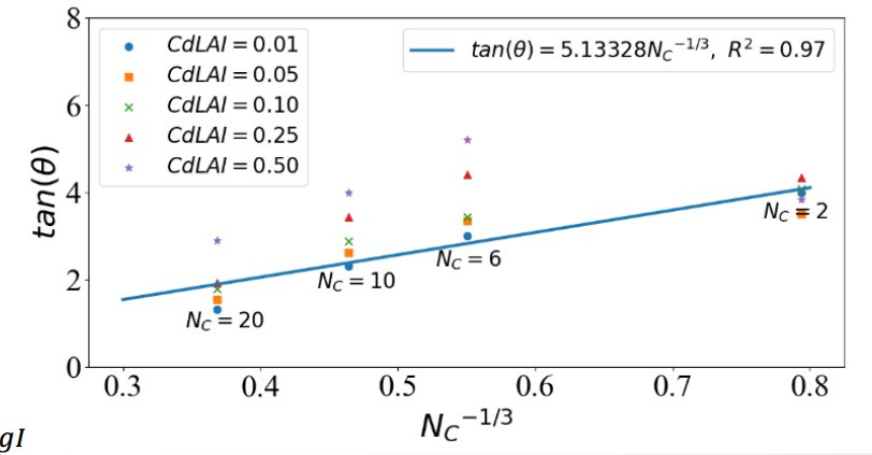
Model correlations	Fuel
$\tan(\theta) = C \times \left(\frac{2T_0}{T_f}\right)^{1/5} \times Ka^{-1/5}$ (1)	Heptane, Ethanol, and Acetone
$\tan(\theta) = \begin{cases} C_1 \times \alpha^{1/2} N_C^{-1/3} & (N_C < 10) \\ C_2 \times \eta^2 N_C^{-2/3} & (N_C > 10) \end{cases}$ (2)	Long leaf pine, slash pine litter, etc.
	(3)

(Hu et al. 2013
 Tang et al. 2015)

(Nelson, 2003)



fitting? ❌



$$\tan(\theta) = C \times \left[2 \times \frac{\rho_0 C_{p,0} T_0 U_0^3}{2gl} \times \frac{U_0^2 T_f}{g(T_f - T_0)D} \times \frac{T_0}{T_f} \right]^{1/5} = C \times \left(\frac{2T_0}{T_f}\right)^{1/5} \times [Ka]^{-1/5}$$

$$\left\{ \begin{aligned} N_C &= \frac{2gl}{\rho_\infty (U_\infty - ROS)^3 C_p T_\infty} \\ R_i &= g\Delta T_f D / T_f U_0^2 \\ K_a &= N_C \times R_i \end{aligned} \right.$$

Interestingly, $Ka^{-1/5} \sim N_C^{-1/3}$, equation (1) and (2) are essentially the same, only applicable to $N_C < 10$, role of CdLAI?

Finding (1)

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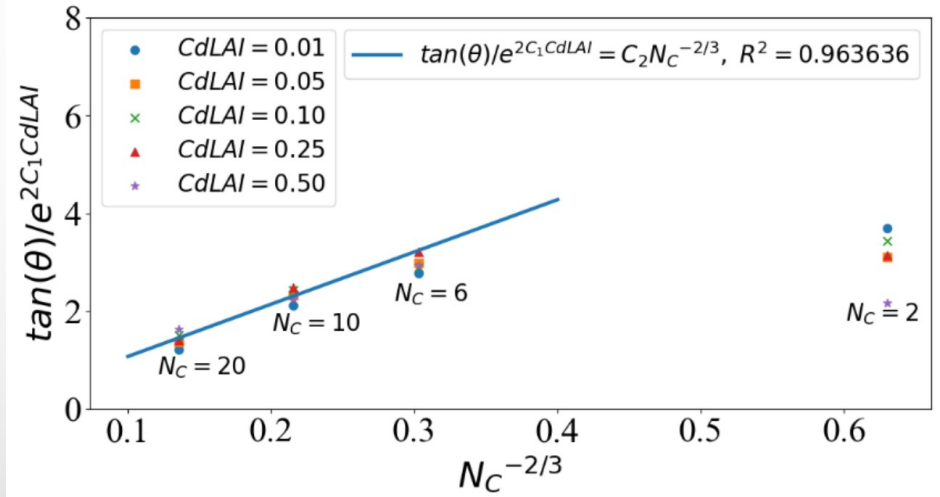
Conclusions

New mathematical correlation is required!



$$\tan(\theta) = \frac{F_d}{F_b} \left\{ \begin{array}{l} \frac{C_d \rho_0 U_e^2 HL}{\rho w_0^2 HL} \sim C_2 \times \eta^2 N_C^{-2/3} \quad (N_C > 10) \quad (3) \quad \text{where } \eta = U_e/U_0 \quad (\text{Nelson, 2003}) \quad \text{Old} \\ \frac{\rho_0 U_e^2 HL}{\rho w_0^2 HL} = \frac{\rho_0 e^{(2C_1 CdLAI)} U_0^2 HL}{\rho w_0^2 HL} = C_2 e^{2C_1 CdLAI} \times N_C^{-2/3} \quad \text{where } \begin{cases} \ln \eta = C_1 CdLAI \text{ or } \eta = e^{(C_1 CdLAI)} \\ U_e = e^{(C_1 CdLAI)} U_0 \end{cases} \quad \text{New} \end{array} \right. \quad (4)$$

Finding (2)



Importance of configuration space $\{N_C, CdLAI\}$ highlighted!

Perfect fitting for $N_C > 10$
 Good fitting for $N_C > 6$

For $C_1 = 0.5366287, C_2 = 10.76685369$

Motivation

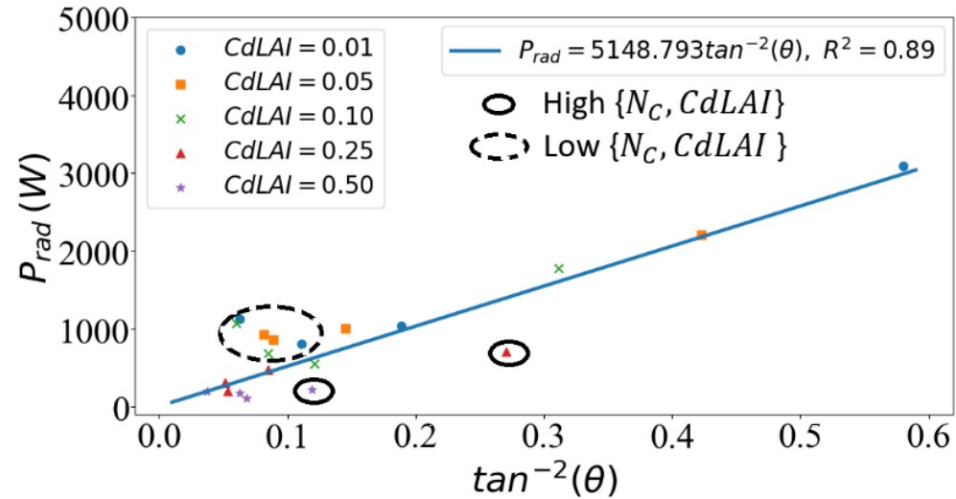
Numerical configuration

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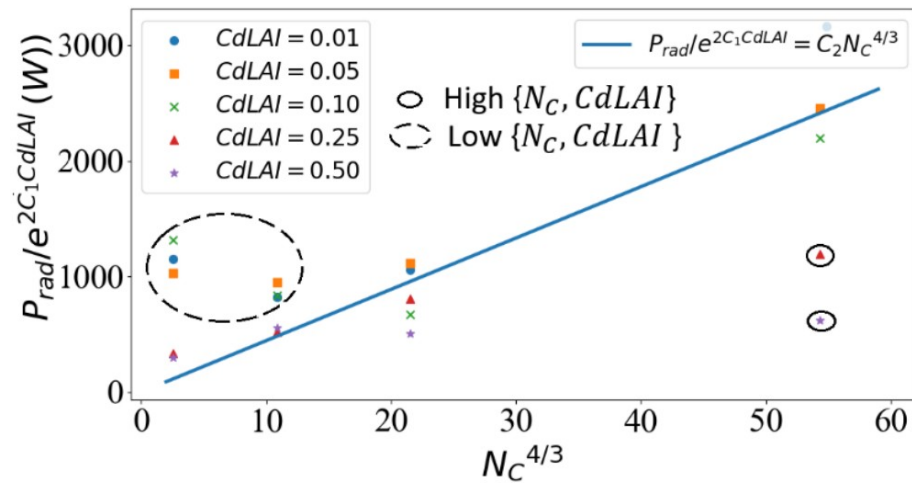
New mathematical correlation is required!



Definition of radiative heat power:

$$P_{rad} = \int Q_{rad}^s dv / CdLAI$$

$$P_{rad} = 5148.793 \tan^{-2}(\theta) \text{ with } R^2 = 0.89$$



$$P_{rad} = C_2 e^{2C_1 CdLAI} N_C^{4/3}$$

With $C_1 = -1.0732574$ and $C_2 = 44.41481$

Motivation

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- Effect of vegetation density ($CdLAI$) is highlighted.
- Flame tile angle \sim directly related to $CdLAI$, inversely related to N_c .
- Radiative heat power \sim directly related to N_c , inversely related to $CdLAI$.
- Fitting with experimental data needed to validate proposed model correlations.



Thank You